DEPARTMENT OF TRANSPORT OPPICE OF ROAD SAFETY

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Title and Subtitle

A Software Package to Identify and Select Treatments for Hazardous Utility Poles

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Abstract

This manual describes a suite of computer programs that identify and evaluate treatments for hazardous roadside utility poles. The program PRANK is used to identify the hazardous poles in the set of poles that is input to it. The program POLFIX is used to evaluate feasible treatments to a small group of utility poles. The cost of each treatment is compared against the expected benefits accruing from a decrease in accident frequency and/or severity. Included in this manual are detailed User Instructions and examples of the program use.

NOTE:

This report is disseminated in the interest of information exchange. The views expressed are those of the author(s) and do not necessarily represent those of the Commonwealth Government.

The Office of Road Safety publishes two series of reports resulting from internal research and external research, that is, research conducted on behalf of the Office. Internal research reports are identified by OR while external reports are identified by CR.

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EXAMPLES OF PROGRAM USE

E.1 An example run of PRANK

This section includes a copy of the prepared data and the output report. The input forms for this run may be found in Section 3 as figures 3.4, 3.5, 3.6, 3.7, 3.8 and 3.9.

10PTNYNYYNB USER MANUAL FOR A POLE ACCIDENT REMEDIAL PROGRAM 20PTN 4, 36 0.00378 0.2 10FOX REPORT 381 PAGES EAST OF PAGE 1. CASE STUDY NUMBER 1. 1MMI IMMS 10 5 5 83 U110U17500450.2 12.40 10 1MMI 20FOX REPORT 385 PAGES EAST OF PAGE 1. CASE STUDY NUMBER 2. THMS 20 42 1250064 0, 75 30FOX REPORT 385 PAGES EAST OF PAGE1. ABOVE POLE AS MJMI. 1MJMI 2MJMI 30 4 2 1250064 0.75 7.4 Y-2.6 T 12 1MJMJ 40HIGH ST 200M SE OF MAIN AVE UTOPIA CITY. **2MJMJ** 40 4 3 1534045 0, 16 N-0.5 T5900 Y 1MINI 50SMITH ST 20M WEST OF BROWN ST SUBURBIA. 2MINI 50 6 5 500, 75 6, 0 1. 0

Prepared Input Data

OPTIONS AND PARAMETERS

RELATIVE RISKS BY POLE CATEGORIES

MNI	4 3€
MINI	0.33
LMLM	7 27
MJMI	0, 65

OFTIONS

REPORT SORTED BY NUMBER OF ACCIDENTS FULL REPORT	T F
UNSORTED REPORT	T
FULL REPORT	T
INCLUDE RECORDED ACCIDENTS	F
SKID TESTER	BPS
CUTOFF NUMBER OF ACCIDENTS @	. 20
POLE/SECOND TRIAL PROBABILITY 0 003	780
PRINT STANDARD DEVIATIONS	Т

UTILITY POLE EXPECTED ROCIDENT RESULTS

MNI	LOCATION: FOX REPORT 381 PAGES EAST OF CONSTRUCTION: RIGID BASE STEEL TOTAL RELATIVE RISK 142.24 SITE VARIABLE	USAGE:	LIGHTING	EXPECTED ACCIDENTS PVA STANDARD DEVIATION = 0.38	8 . 53768
	ABSOLUTE MAXIMUM CURVATURE	6.0120	3. 11		
	AADT	17500.	1, 24		
	SKID TEST	45	1. 50		
	LATERAL OFFSET	6 , 26	1. 38		
	WIDTH DISTANCE FROM CURVE START	12. 4 110	* 1. 32 1. 18	•	
	POLE ON INSIDE OF CURVE	0UT	1. 15		
	PAVEMENT DEFICIENCIES	CORR	2.00		
	SUPERELAVATION	EAD	1, 20		
INI	LOCATION: FOX REPORT 385 PAGES EAST OF CONSTRUCTION: RIGID BASE TIMBER TOTAL RELATIVE RISK 2.18 SITE VARIABLE	USAGE: DEGPEE (VALUE	ELECTRICAL CONDUCTOR OF SHIELDING Ø RELATIVE RISK	NUMBER 20. EXPECTED ACCIDENTS P/A STANDARD DEVIATION = 0.00	8. Ø0S23
	ABSOLUTE MAXIMUM CURVATURE	9. 8888	9. 60		•
	AADT	12560.	1. 94		
	SKID TEST	64	6. 78		
	LATERAL OFFSET	0, 75	1, 23		
	WIDTH	UNSF	1. 00		
	DISTANCE FROM CURVE START	UNSP	1. 00	- · ·	
	POLE ON INSIDE OF CURVE	UNSF	1. 00	- · · · · · · · · · · · · · · · · · · ·	
	PAVEMENT DEFICIENCIES	NONE	0. 93		
	SUPERELAVATION	UNSF	1, 00		
JMI	TOTAL RELATIVE RISK 0.18	USAGE:	ELECTRICAL CONDUCTOR OF SHIELDING O RELATIVE RISK	NUMBER 30 EXPECTED BCCIDENTS PZA STANDARD DEVIATION = 9.00	9. 99945
	SITE VARIABLE				
		12500			
	AADT	18500.	Ø. 6 8		
	AADT SKID TEST	18500. 64	0. 68 0. 65		
	AADT SKID TEST LATERAL OFFSET	18500. 64 0.75	0. 68 0. 65 1. 42		
	AADT SKID TEST	18500. 64	0. 68 0. 65		

-2.60

TEE

1£.

1.03

0.70

1.04

GRADE 30M UPSTREAM OF INTERSECTION

RADIAL DISTANCE FROM INTERSECTION

INTERSECTION TYPE

24-NOV-80

UTILITY FOLE EXPECTED ACCIDENT RESULTS

мјмј	LOCATION: HIGH ST 200M SE OF MAIN AVE U CONSTRUCTION: RIGID BASE TIMBER TOTAL RELATIVE RISK 5.01 SITE VARIABLE	USAGE: L.	IGHTING & CONDUCTOR SHIELDING Ø RELATIVE RICH	EXPECTED F		S F/A		0. 01893
		15340.		_				
	SKID TEST	45	1 15	-				•
		0. 20	1. 28					
	THROUGH ROADWAY DIVIDED	NO	1.00					£
	GRADE 3GM UPSTREAM OF INTERSECTION		0 . 86					₹.
	INTERSECTION TYPE	TTL						
	AADT INTERSECTING ROADWAY	5900 uza	0, 63	_				
	INTERSECTING PORDWAY DIVIDED TRAFFIC LIGHTS	YES YES	1, 60	3				
HINI	LOCATION: SMITH ST 20M WEST OF BROWN ST CONSTRUCTION: RIGID BASE CONCRETE TOTAL RELATIVE RISK 0.42 SITE VARIABLE	USAGE: DEGREE OF VALUE	LIGHTING	EXPECTED A		S F/A		0. 0015 8
WINI	CONSTRUCTION: RIGID BASE CONCRETE TOTAL RELATIVE RISK 0.42	USAGE: DEGREE OF	LIGHTING SHIELDING 0	EXPECTED A STANDARD D	ACCIDENT:	S F/A		ø. 90158
MINI	CONSTRUCTION: RIGID BASE CONCRETE TOTAL RELATIVE RISK 0.42 SITE VARIABLE	USAGE: DEGREE OF VALUE 0. 0000 UNSP	LIGHTING SHIELDING 0 RELATIVE RISE	EXPECTED A STANDARD D C	ACCIDENT:	S F/A		0. 00158
MINI	CONSTRUCTION: RIGID BASE CONCRETE TOTAL RELATIVE RISK 0.42 SITE VARIABLE	USAGE: DEGREE OF VALUE 0.0000	LIGHTING SHIELDING 0 RELATIVE RIST	EXPECTED A STANDARD D C - 3	ACCIDENT:	S F/A		0. 00158
MINI	CONSTRUCTION: RIGID BASE CONCRETE TOTAL RELATIVE RISK 0.42 SITE VARIABLE	USAGE: DEGREE OF VALUE 0. 0000 UNSP 50	LIGHTING 9 SHIELDING 9 RELATIVE RIST	EXPECTED F STANDARD E C - 3	ACCIDENT:	S F/A		0. 00158
WINI	CONSTRUCTION: RIGID BASE CONCRETE TOTAL RELATIVE RISK 0.42 SITE VARIABLE	USAGE: DEGREE OF VALUE 0. 0000 UNSP 50	LIGHTING 8 SHIELDING 8 RELATIVE RISH 0.60 1.00 2.94	EXPECTED A STANDARD C C C C C C C C C C C C C C C C C C C	ACCIDENT:	S F/A	0. 00	0. 001 5 8

UTILITY POLE RISKS SORTED BY EXPECTED ACCIDENTS

24-NOV-80

MNI LOCATION: FOX REPORT 381 PAGES EAST OF PAGE 1. CASE STUDY NUMBER 1. NUMBER 10 CONSTRUCTION: RIGID BASE STEEL USAGE: LIGHTING EXPECTED ACCIDENTS P/A 0,53766 TOTAL RELATIVE RISK 142.24 DEGREE OF SHIELDING 10 STANDARD DEVIATION = 0.38 MJMJ LOCATION: HIGH ST 200M SE OF MAIN AME UTOPIA CITY. NUMBER CONSTRUCTION: RIGID BASE TIMBER USAGE LIGHTING & COMMUNITOR EXPECTED ACCIDENTS FUR TOTAL RELATIVE RISK 5.01 DEGREE OF SHIELDING G STANDARD DEVIATION = 0.02

> ACCEPTED RECORDS = ERROR RECORDS = TOTAL RECORDS

E.2 An example run of POLFIX

This section includes a sample batch of input forms, a copy of the prepared data and the output report. Note that usage of the input forms results in a large amount of paper being used. When the user is familiar with the package he may elect to code directly onto coding forms.

```
10PTN USER MANUAL FOR H FOLE ACCIDENT REDSCRIPE FROGRAM
20PTN 10 0PB

1SITE 7 PROUNCYTELE SUITH ST 100N FA:3 OF JUNES ST
10NNI 7 1 5 5 0 2500050 0 7512 50

10NNI 7 3 5 5 00012002500040 0 7512 50

11PRT 1 3 PELOCATE ALL POLES TO A LATERAL OFFSET OF 2 5M
21PFT 3

1TEFF 7 1 2 5 5
1TEFF 7 3 2 5 5
1TPRT 2 CONVERT POLES 2 AND 3 TO WRAP AROUND CONSARUCTION
21PRT 2 9
1TEFF 7 3 9
1TPRT 2 CONVERT PENAINING POLE TO WRAP AROUND
21PRT15800 1
1TEFF 7 3 9
```

Prepared Input Data

1 TO P TN

-94-

			HEADING FOR OUTP	υτ	•	
ा जडा	RIMANDALIA	AR A POLE	ACCIDENT	REMEDIAL PR	OGRAM	
6	16	. 26	36	46	56	
		RELAT	IVE RISK BY POLE	CATEGORIES		
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1	. •					
	MAJOR ROAD		NOR ROAD	MAJOR/MAJOR	MAJOR	VMINOR
	NON INTERSECTION	·	N INTERSECTION	INTERSECTION	ן וואובו	SECTION
	.6	11		16	21	
	•			SKID TESTER		
	ACCIDENT FACTOR		INTEREST RATE	B'= BPS S = SCRIM	RANK E	Y B/C RATIO =
			10.0	S - Scient	_	(1) (B)
	26	. 3		38		39
	PRINT POLE DESC. Y or N	•	PRINT TREATMENT EFFECT DETAILS			
	<u> </u>					
	40	•				
						
			LE SITE TREATMEN			POL-2
		SITE	DESCRIPTION FO	DRM.		
1 S +	T	SITE NUMBER		SITE BUDGET		
1	ale.	6	10	12	18	
	_		SITE DESCRIPTION			
 जिल्लासम्ब	SVIII SOL	नाम रिन्हिंगिर्ग	ार्यक्रा सिन्	राज्यास्य गरावस्य	REFER F.A	7 17 2
18 [Livinia]	29 -	3 9	49	59	69	

MAJOR ROAD NON-INTERSECTION POLE DESCRIPTION

1 DMN I	-95	-		
SITE POLE MIMBER NUMBER 6 10 12	CONSTRUCTION USAGE S S S 17	MINIMIM RADIUS OF CURVE 0 18	POLE ON INSIDE(N) OR OUTSIDE (U) OF CURVE	DISTANCE FROM CURVE START
SUPER- ELEVATION (F or U) AADT 26 27	SKID LATERAL TEST OFFSET SO 0:7 32 34	ROAD WIDTH ショフター マンス・マンス・マンス・マンス・マンス・マンス・マンス・マンス・マンス・マンス・	PAVEMENT DEFICIENCIES (N,T,D,C) A3	44
45 50	51	56 57		60
·	UTILITY POLE SITE 1			POL-S
1 DM N 1		- DESCRIPTION		
SITE POLE NUMBER NUMBER 6 10 12	CONSTRUCTION USAGE	MINIMUM RADIUS OF CURVE	POLE ON INSIDE(N) OR OUTSIDE (U) OF CURVE U 22	DISTANCE FROM CURVE START 4 0.
SUPER- ELEVATION (F or U) AADT U \[\lambda \sum 0 0 0 \] 26 27	SKID LATERAL OFFSET 45 0.7 32 34	ROAD WIDTH S 12-5 39	PAVEMENT DEFICIENCIES (N,T,D,C) C 43	44
45 50	51	56 57	,	. 60

MAJOR ROAD NON-INTERSECTION POLE DESCRIPTION

1 DIM NI I	-9	0-			
SITE POLE NUMBER NUMBER 0 1 7 3 1	CONSTRUCTION USAGE 13 15 17	MINIMUM RADIUS OF CURVE 60	POLE ON INSIDE(N) OR OUTSIDE (U) OF CURVE 22	DISTANCE FROM CURVE START 120	•
SUPER- ELEVATION (F or U) AADT 25 00 0 26 27	SKID LATERAL OFFSET 4-0 0.7 32 34	ROAD WIDTH 12.5	PAVEMENT DEFICIENCIES (N,T,D,C) C 43	44	
45 50	51	56 5		60	
	MITTLE SOLE SITE	TREATMENT PROGRAM		POL-3	_
	TREATMENT D	ESCRIPTION		FOL-3	
ALTERNA MIMBER 1 T PR T 6	TIVE 8	TREATMENT CODE	11		
	DESCRIPTION O	F TREATMENT			
TRELOCATE ALL PO	도 등 1 1 시 주 1 기		62	SMITT	
SERVICE	CADYTAL				
LIFE 6	CAPITAL COST/UNIT	NUMBER UNITS 3	OF AN CO	NUAL ST	

TREATMENT EFFECT FORM

Only fill in fields that have changed

<u>1 </u>	-97-	*	•
SITE POLE NUMBER CONSTRUCT 6 10 12 13	FION USAGE OF CURVE 15 17 18	POLE ON INSIDE(N) OR OUTSIDE (U) OF CURVE	DISTANCE FROM CURVE START 23
SUPER- ELEVATION SKID (F or U) AADT TEST	LATERAL ROAD OFFSET WIDTH	PAVEMENT DEFICIENCIES (N,T,D,C)	ROADWAY 1 DIVIDED
26 27 32 AAD INTERSECTION INT GRADE TYPE(X or T) ROA	ERSECTING ROADWAY RADI	43 IAL DISTANCE INTO	44 ERSECTION CONTROLLED
√5 50 51		I INTERSECTION, BY 5	FRAFFIC LIGHTS 60
···	TREATMENT EFFECT FORM fill in fields that have changed	=	POL-4
SITE POLE NUMBER NUMBER CONSTRUCT 6 10 12 13	ION USAGE OF CURVE 15 17 18	POLE ON INSIDE(N) OR OUTSIDE (U) OF CURVE 22	DISTANCE FROM CURVE START
SUPER- ELEVATION SXID (F or U) AAUT TEST 26 27 32	LATERAL ROAD WIDTH	PAVEMENT DEFICIENCIES (N,T,D,C) 1 43	ROADWAY 1 DIVIDED
GRADE INTERSECTION INTERSECTION INTERSECTION FOAD TYPE(X of T) ROAD 5 50 51	RSECTING ROADWAY RADIL WAY DIVIDED FROM	AL DISTANCE INTE INTERSECTION, BY T	RSECTION CONTROLLED RAFFIC LIGHTS 60

TREATMENT EFFECT FORM

Only fill in fields that have changed

1 TE FF	Unity fill in fields	that have changed			
1	-98-		·		
SITE POLE NUMBER NUMBER 6 10 12	CONSTRUCTION USAGE 13 15 17	MINIMUM RADIUS OF CURVE	POLE ON INSIDE(N) OR OUTSIDE (U) OF CURVE	DISTANCE FROM CURVE START 23	
SUPER- ELEVATION (F or U) AAUT 26 27	SKID LATERAL DEFESET	ROAD WIDTH 39	PAVEMENT DEFICIENCIES (N,T,D,C)	ROADWAY 1 DIVIDED L 44	
GRADE INTERSECT TYPE(X or 50	ION INTERSECTING ROA		INTERSECTION, BY	ERSECTION CONTROI TRAFFIC LIGHTS 60	LED
			·		
	VILLITY POLE SITE TO			POL-3	
	TREATMENT DE	SCRIPTION			
ALTERNATI MANBER 17 PRT 6	8	TREATMENT CODE	11		
	DESCRIPTION OF	TREATMENT			
<u> </u>	32 42	로 이 이 시 이 시 이 시 S T 52	यिपयमान्य 62		
TPRT		•			
· ,					
SERVICE LIFE //S	CAPITAL COST/UNIT 8 0 0 1	NUMBER OUNITS		NMIAL DST	

TREATMENT EFFECT FORM

Only fill in fields that have changed

			•	
	-99	-	•	
			DOLD ON THE TOP (1)	
SITE_ POLE		MINIMIM RADIUS	POLE ON INSIDE (N) OR OUTSIDE (U)	
NUMBER NUMBER CONSTRUCTI	ON USAGE	OF CURVE	OF CURVE	START
<u> </u>			W	
6 10 12 13	15 17	18	. 22	23
		w 1		
		:	•	
SUPER-	•	•		
ELEVATION SKID	LATERAL	ROAD .	PAVEMENT DEFICIENCIES	ROADWAY 1
(F or U) AADT TEST	OFFSET	. WIDTH	(N,T,D,C)	DIVIDED
]		
26 27 32	34	39	43	44
			٠.	
•				
•	-		•	
AADT INTERSECTION INTE		TERSECTION	1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
GRADE TYPE(X or T) ROAD			U. DISTANCE IN INTERSECTION, BY	TERSECTION CONTROLLED TRAFFIC LIGHTS
			<u> </u>	\Box
45 50 51		56	57	. 60
•				
	•. •			•
••				•
				
ÀIÌTÌ	TY POLE SITE TI	LEATMENT PROGRAM		POL-4
	TREATMENT EF	FCT FORM		
				
	till in fields i	hat have changed		
11 11 12 2 2				
1 TE FF			<u>-</u>	
1 TE FF			·	
1 TE FF				
			POLE ON INSIDE(N)	DISTANCE
SITE POLE		MINIMUM RADIUS	POLE ON INSIDE(N) OR COUTSIDE (U)	DISTANCE FROM CURVE
SITE POLE NUMBER CONSTRUCTIO			POLE ON INSIDE(N) OR OUTSIDE (U) OF CURVE	
SITE POLE NUMBER NUMBER CONSTRUCTIO	ON USAGE	MINIMUM RADIUS OF CURVE	OR OUTSIDE (U) OF CURVE	FROM CURVE START
SITE POLE NUMBER CONSTRUCTION - 7 3 7 9	ON USAGE	MINIMUM RADIUS	OR OUTSIDE (U)	FROM CURVE
SITE POLE NUMBER NUMBER CONSTRUCTIO	ON USAGE	MINIMUM RADIUS OF CURVE	OR OUTSIDE (U) OF CURVE	FROM CURVE START
SITE POLE NUMBER NUMBER CONSTRUCTIO	ON USAGE	MINIMUM RADIUS OF CURVE	OR OUTSIDE (U) OF CURVE	FROM CURVE START
SITE POLE NUMBER NUMBER CONSTRUCTIO - 7 3	ON USAGE	MINIMUM RADIUS OF CURVE	OR OUTSIDE (U) OF CURVE 22	FROM CURVE START
SITE POLE NUMBER NUMBER CONSTRUCTION 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	IN USAGE 15 17 LATERAL	MINIMUM RADIUS OF CURVE 18 ROAD	OR OUTSIDE (U) OF CURVE 22 PAVEMENT DEFICIENCIES	FROM CURVE START 23
SITE POLE NUMBER NUMBER CONSTRUCTIO - 7 3	ON USAGE	MINIMUM RADIUS OF CURVE	OR OUTSIDE (U) OF CURVE 22 PAVEMENT	FROM CURVE START
SITE POLE NUMBER NUMBER CONSTRUCTION	USAGE 15 17 LATERAL OFFSET	MINIMUM RADIUS OF CURVE 18 ROAD WIDTH	PAVEMENT DEFICIENCIES (N,T,D,C)	FROM CURVE START 23 ROADWAY 1 DIVIDED
SITE POLE NUMBER CONSTRUCTIO 7 3	IN USAGE 15 17 LATERAL	MINIMUM RADIUS OF CURVE 18 ROAD	OR OUTSIDE (U) OF CURVE 22 PAVEMENT DEFICIENCIES	FROM CURVE START 23
SITE POLE NUMBER NUMBER CONSTRUCTION	USAGE 15 17 LATERAL OFFSET	MINIMUM RADIUS OF CURVE 18 ROAD WIDTH	PAVEMENT DEFICIENCIES (N,T,D,C)	FROM CURVE START 23 ROADWAY 1 DIVIDED
SITE POLE NUMBER NUMBER CONSTRUCTION	USAGE 15 17 LATERAL OFFSET	MINIMUM RADIUS OF CURVE 18 ROAD WIDTH	PAVEMENT DEFICIENCIES (N,T,D,C)	FROM CURVE START 23 ROADWAY 1 DIVIDED
SITE POLE NUMBER NUMBER CONSTRUCTIO 1 17 13 1 19 6 10 12 13 SUPER- ELEVATION (F or U) AADT TEST 26 27 32	IN USAGE 15 17 LATERAL OFFSET 34	MINIMUM RADIUS OF CURVE 18 ROAD WIDTH 39	PAVEMENT DEFICIENCIES (N,T,D,C)	FROM CURVE START 23 ROADWAY 1 DIVIDED
SITE POLE NUMBER NUMBER CONSTRUCTION 6 10 12 13 SUPER- ELEVATION (F or U) AADT TEST 26 27 32 AADT INTERSECTION INTERS	LATERAL OFFSET 15 17 IATERAL OFFSET INT. SECTING ROA	MINIMIM RADIUS OF CURVE 18 ROAD WIDTH 39 ERSECTION DWAY RADIAI	PAVEMENT DEFICIENCIES (N,T,D,C) 43	FROM CURVE START 23 ROADWAY 1 DIVIDED 44 ERSECTION CONTROLLED
SITE POLE NUMBER NUMBER CONSTRUCTION 6 10 12 13 SUPER- ELEVATION (F or U) AADT TEST 26 27 32 AADT	LATERAL OFFSET 15 17 IATERAL OFFSET INT. SECTING ROA	MINIMIM RADIUS OF CURVE 18 ROAD WIDTH 39 ERSECTION DWAY RADIAI	PAVEMENT DEFICIENCIES (N,T,D,C) 43	FROM CURVE START 23 ROADWAY 1 DIVIDED 44
SITE POLE NUMBER NUMBER CONSTRUCTION 6 10 12 13 SUPER- ELEVATION (F or U) AADT TEST 26 27 32 AADT INTERSECTION INTERS	LATERAL OFFSET 15 17 IATERAL OFFSET INT. SECTING ROA	MINIMIM RADIUS OF CURVE 18 ROAD WIDTH 39 ERSECTION DWAY RADIAI	PAVEMENT DEFICIENCIES (N,T,D,C) 43 DISTANCE INTERSECTION BY	FROM CURVE START 23 ROADWAY 1 DIVIDED 44 ERSECTION CONTROLLED

TREATMENT DESCRIPTION

-100- ALTERNATIVE TREATMENT
MMBER CODE
1 6 8 9 11
DESCRIPTION OF TREATMENT
COMVERTIME MAILMAN AOLE TO WARP MADUMO
12 22 .32 42 52 62
2T PR T
1
SERVICE CAPITAL NUMBER OF ANNUAL
LIFE COST/UNIT UNITS COST
6 8 15 20
UTILITY POLE SITE TREATMENT PROCRAM POL-4
TREATMENT EFFECT FORM
Only fill in fields that have changed
1 TE FF
POUR ON THE TREE PROPERTY.
SITE POLE POLE ON INSIDE(N) DISTANCE MUMBER CONSTRUCTION USAGE OF CURVE OF CURVE START POLE ON INSIDE(N) DISTANCE OF CURVE OF CURVE START
6 10 12 13 15 17 18 22 23
SUPER- FI EVATION PAVEMENT
ELEVATION SKID LATERAL ROAD DEFICIENCIES ROADWAY 1 (F or U) AADT TEST OFFSET WIDTH (N,T,D,C) DIVIDED
26 27 32 34 39 43 44
AAUT INTERSECTION
GRADE INTERSECTION INTERSECTING ROADWAY RADIAL DISTANCE INTERSECTION CONTROLLED FROM INTERSECTION, BY TRAFFIC LIGHTS
45 50 51 56 57 60

23-DEC-80

PROGRAM PARAMETERS

PELATIVE RISK TO ACCIDENT FACTURE 0.00770 POLATIVE RISK BY FOLE CATEGORY, MHI 4.3-0 33 MINI 7. 27 MIMJ - liJnJ (1. €· →• INTEREST RATE 10. 00 EVALUATE ALTERNATIVES BY 8.70 SKID TESTER E:PS PRINT POLE DESCRIPTIONS 4 PRINT TRIERTMENT EFFECT DETAILS Ψ PRINT STANDARD DEVIATIONS

101-

SITE: PROWNSVILLE, SMITH ST. 120M EAST OF JONES ST.

SITE NUMBER: 7. SITE BUDGET # 8

FOLE NO.		MAXIMUM CURVATURE					DISTANCE FROM CURVE START				TOTAL RR	
1 RE:	MNI 4.36	9, 909 9, 69	25000. 1. 33	50 1. 10	6, 75 1, 83	12, 5 1, 30	-1 1. 00	UNSP 1, 6 0	NONE 6, 93	UNSF: 1, 00	5. 69	
					USAÇE:		EIGHTING EXPECTED ACCIDE					
		MAXIMUM CURVATURE			LATERAL	ROND	DISTANCE FROM CURVE START	INSIDEZ	PAVEMENT	S-UF-EF	TOTAL	
2 RR: CONS ACCI	4, 36 TRUCTI	7.40 ++ ON: RIG	1.33 ID BASE	1, 50 ++ STEEL	1, 23 ++ U\$AGE:	1 30	40 1.55 ++ LIGHTING EMPECTED ACCIDE	1, 15 ++ EXF	2.00 ++ ECTED ACCIDENT	1, 20 ++ '3 F/A: 1. (440.30 6665418 ON =	1 04
POLE NO.		MAXIMUM CURVATURE			LATERAL	F:OAD	DISTANCE FROM CURVE STAPT	INSIDEZ	PAVEMENT	SUPER-	TOTAL	
3 RR:	MNI 4. 36	0 017 7.40 ++	25000. 1. 33	49 1, 89 ++	0, 75 1, 23 ++	12.5 1 30	120 1.05 LIGHTING	OUT 1, 15	COFR 2 00 ++	BAD ; 1, 20	376, 88	
CONS	TRUCTI DENT C	ON RIG	IO BASE S POLE T	STEEL YPE = #	USAGE 12495. C	40 T&O.	LIGHTING EXPECTED ACCIDE	EXF NTS = \$ 1	ECTED ACCIDENT 7884 STANDA	S PYR 1. ARD DEVIATIO	4264911 DN =	1 1 8

TOTAL NUMBER OF ACCIDENTS EXPECTED PER SITE 3 11 STANDARD DEVIATION = 1.57 TOTAL COST \$ 38917.

```
TREATMENT ALTERNATIVE NUMBER 1
```

TREATMENT PART NUMBER: 1 FELOCATE ALL POLES TO A LATERAL OFFSET OF 2 SM

POLE 1 LATERAL OFFSET CHANGED TO 8.50 NEW RELATIVE RISK 0.58
POLE 8 LATERAL OFFSET CHANGED TO 8.50 NEW RELATIVE RISK 0.58
POLE 3 LATERAL OFFSET CHANGED TO 8.50 NEW RELATIVE RISK 0.50
NEW EXPECTED NUMBER OF ACCIDENTS PVA FOR SITE 1.3167 CHANGE = -1.7970
SERVICE LIFE 15 YEARS CAPITAL COST \$ 150. DISCOUNTED BENEFITS 1 99072.

NET PRESENT VALUE # 96178 BENEFIT/COST RATIO = 68.45 STANDARD DEVIATION = 85.10

EFFECTS OF BUTEFNATIVE NUMBER 4

PARTS INCLUDED:

NEW EXPECTED NUMBER OF ACCIDENTS FOR SITE 1.31673 CHANGE = -1.79784

TOTAL CAPITAL COST \$ 1500. TOTAL BENEFITS \$ 93672.

NET PRESENT VALUE \$ 92172. BENEFIT/COST FATIO 62,45 STANDARD DEVIATION \$ \$5.10

TREATMENT ALTERNATIVE NUMBER &

TREATMENT FART NUMBER 2 CONVERT POLES 2 AND 3 TO WRAP AROUND CONSTRUCTION

POLE 2 CONSTRUCTION CHANGED TO WRAP AROUND NEW ACCIDENT COST = 1 2380.
FOLE 3 CONSTRUCTION CHANGED TO WPAP AROUND NEW ACCIDENT COST = 1 2380.
MEW EXPECTED NUMBER OF ACCIDENTS PZA FOR SITE 3.1146 CHANGE = 0.00000 The SERVICE LIPE 15 YEARS CAPITAL COST 1 1600 DISCOUNTED BENEFITS 1 170459.
MET PRESENT VALUE 1 18859. BENEFITZOST RATIO = 81.54 STANGARD DEVIATION = 46.91

TREATMENT PART NUMBER - 3 CONVERT REMAINING FOLE TO WHAP APOUND

POLE 1 CONSTRUCTION CHANGED TO NAME AROUND NEW ACCIDENT COST ≈ # 2280

UTILITY FOLE SITE TREATMENT PROGRAM

NEW EXPECTED NUMBER OF ACCIDENTS PVH FOR SITE 3.1146 CHANGE = 0.0000
SERVICE LIFE 15 YEARS CAPITAL COST : 800 DISCOUNTED BENEFITS : 909.
NET PRESENT VALUE : 109. BENEFIT/COST RATIO = 1.14 STANDARD DEVIATION = 66.30
** TREATMENT ACCEPTED **

EFFECTS OF ALTERNATIVE NUMBER

PARTS INCLUDED.

É.

NEW EXPECTED NUMBER OF ACCIDENTS FOR SITE, 3 11457 CHANGE.= 0.00000

TOTAL CAPITAL COST : 2400. TOTAL BENEFITS : 131367.

NET PRESENT VALUE # 128967 BENEFIT/COST RATIO | 54,74 | STANDARD DEVIATION = | 38,29

Validation

RESULTS FOR SITE 7.

ALTERNATIVE	EXPECTED	CAPITAL	TOTAL	NET PRESENT	BENEFITZCOST	STANDARD
NUMBER	ACCIDENTS FZA	COST	SENEFITS	VALUE	RATIO	DEVIRTION
1 2	1. 3167	≴ 1500.	# 93672.	1 92178	62 45	85. 10
	3. 1146	≴ 2400	# 131367.	1 128967	54 74	38. 29
ς.	S. 1140	4 64600.	# #0#0D()	4 正になけれて、	2'\$ (4	30 C.T

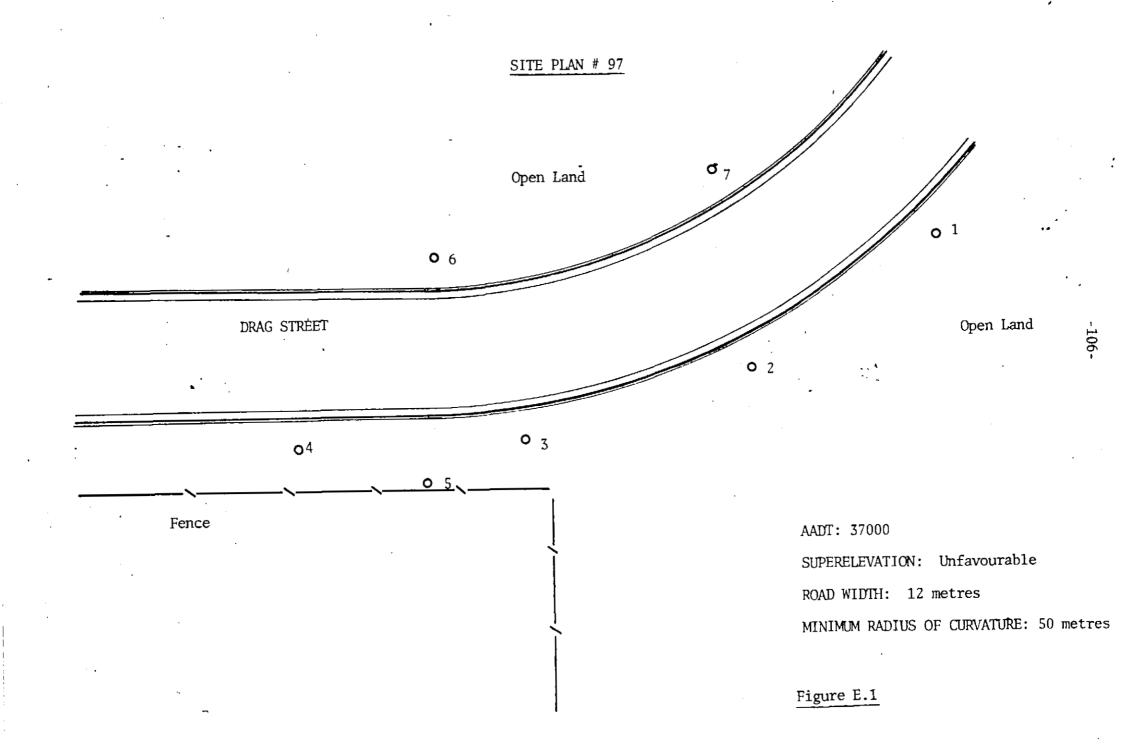
. . .

E.3 A further example of POLFIX

This section shows the preferred input data for a treatment site, the site plan and the POLFIX output. Some points to note are:

- o Poles on both sides of the road have been included because one of the possible treatments is road resurfacing.
- o Pole number five has been included so that the full benefits or road resurfacing will be shown i.e. the reduction in the accident risk of the fence is included in the benefits.
- o When the poles on the outside of the curve are removed, poles 3 and 4 are changed to 'Fence Equivalent' instead of being totally removed. This is done on the assumption that cars that would have hit poles 3 and 4, will now hit the fence.

```
1 OF TH
        POLAME USER MANUAL - A FURTHER POLETX EXAMPLE
20PTN
                    HAIRY CORNER ON DRAG STREET - SEE PLAN #97
1SITE
             4 8 50 U 30U3700040 0.25 18 N
4 8 50 U 60U3700040 0.85 18 N
         91
1DMNI
10/1/J
         9 2
         9 3 4 2 50 U 90U3700040 G 25 12 C
1DINI
1DINI
         9 4
              4 2 50 U120U3700040 0 25 12 C
1bmi1
                    50 U105U3700040 3.00 18 C
        9 6 5 5 50 N 5003700035 1.0 12 N
9 7 5 5 50 N 9003700035 1.0 12 N
1DHHT
1DMHI
            RESUPPACE DRAG STREET AT HAIFY CORNER
1TPF:T 1
         3.50 2250
ETFRT10
        9 1
1TEFF
         9 2 7
1TEFF
                                   ÉÜ
1TEFF
                                   6.01
1TEFF
           4
                                   ÉŪ
1TEFF
         9 5
                                   6.63
          €
?
1TEFF
                                   60
1TEFF
ITERT 2
            REMOVE ALL POLES ON THE OUTSIDE OF HAIRY CORNER
2TPRT15 5500
1TEFF
         913
         9 2 3
1TEFF
1TEFF
         932
                                     4. 5
1TEFF
                                     2. 5
1TPRT 3 2
           INCREASE THE LATERAL OFFSET OF POLES 3 & 4
ETFRT
1TEFF
         9-3
                                     3. 0
1TEFF
                                     2.5
1TPRT 3 2
           INCREASE THE LATERAL OFFSET OF POLES 1 & 2
STERT
         9 1
1TEFF
         9 2
1TEFF
                                     3. 6
```



PROGRAM PARAMETERS

PELATIVE RISK TO ACCIDENT FACTOR	R:	0 00376
RELATIVE RISK BY POLE CATEGORY	MNI	4.36
	MINI	0.33
	MJMJ	7. 27
	MJMI	0.65
	•	
INTEREST RATE		10.60
EVALUATE ALTERNATIVES BY		B/C
SKID TESTER		BFS
PRINT FOLE DESCRIPTIONS		Y
PRINT TRIEATMENT EFFECT DETAILS		Y
PRINT STANDARD DEVIATIONS		٧

-10/

:

SITE: HAIRY CORNER ON DRAG STREET - SEE PLAN #97 SITE NUMBER: 9.

SITE BUDGET # 0.

POLE NO.							DISTANCE FROM CUEVE START					
1 RF:	MN1 4. 36	9, 920 7, 49	37000. 1. 33	40 1. 69	6, 25 1, 37	18.0 1.75	30 1,55 ++ L CONDUCTOR	OUT 1.15	NONE 0. 93	BAD 1, 20	298. 9 1	
CONS ACCI	DENT C	OST FOR THI	S POLE T	YPE = 1	15539. 0	OST OF	EXPECTED ACCIDE	NTS ≈ 1 1	7637. STANDA	RO DEVIATI	D11 ₽	0 52
NO	POLE TYPE	MAXIMUM CURVATURE	ABDT	SKID TEST	LATERAL OFFSET	ROAD MIDTH	DISTANCE FROM CURVE START	INSIDE/ OUTSIDE	PAVEMENT DEFICIENCIES	SUPER- ELAVATION	TOTAL RR	
e RR:	MNI 4. 36	9. 020 7. 40	37666. 1. 33	40 1. 89	0, 25 1, 37	12. 0 1. 35	60 1.48 ++ IL CONEUCTOR	0UT 1. 15	NONE 6. 93	8AD 1. 20	285 09	
CONS	DENT C	OST FOR THI	S POLE T	YPE = \$	15589. 0	OST OF	L CONSUCTOR EXPECTED ACCIDE	NTS = # 1	.6822. STANDA	RD DEVIRTI	ON =	0, 53
POLE NO.	POLE	MAXIMUM	በ ብርነፕ	SKID	LATERAL	ROND	DISTANCE FROM CURVE START	INSIDE/	PRVEMENT	SUPER-	TOTAL	
3 RR:	MNI 4. 36	9, 929 7, 49	37090. 1, 33	40 1, 89	0, 25 1 37	12 0 1.35	90 1. 26 IL CONDUCTOR	0UT 1.15	CORR 2, 00	BAD 1 ខ្ពស់	583, 94	
CONS ACCI	TRUCTI DENT C	ON: RIGI	D BASE T S POLE T	+4 IMBER YPE ≃ \$	USAGE: EL 15589. C	ECTRICA OST OF	L CONDUCTOR EXPECTED ACCIDE	EXP NTS = 1 3	ECTED ACCIDENT 0915. STANDA	S PVA: 1 : IRD DEVIATIO	9830983 (N =	1. 31
POLE NO	POLE TYPE	MAXIMUM	AADT	SKID	LATERAL	ROBD	DISTANCE FROM CURVE START	INSIDE/	PAVEMENT	SUPERH	TOTAL	
4 RR:	MNI 4.36	0, 020 7, 40	37000. 1, 33	40 1, 89	6. 25 1. 37	12. 0 1. 35	180 1. OS SL CONDUCTOR	OUT 1. 15	CORR 2 00	ВНD 1. 20	435. 9 8	
CONS ACCI	DENT C	OST FOR THI	S POLE T	YFE = #	15589. C	:08T 0F	EXPECTED ACCIDE	NTS = \$ 2	5721. STANDA	RD DEVIATI	DN =	1. 27
NŪ.	POLE TYPE	MAXIMUM CURVATURE	AADT:	SKID TEST	LATERAL OFFSET	ROAD WIDTH	DISTANCE FROM CURVE START	INSIDE/ OUTSIDE	PRVEMENT DEFICIENCIES	SUPER- ELAVATION	TOTAL RE	· -
5 PR:	MNI 4 36	0, 020 7, 40	37000. 1, 33	40 1. 89	3 00 0.47	12. 0 1. 35	105 1.16 NOTHING	OUT 1.15	CORR 2 00 ++	BAD 1, 20	164 45	
CONS RCCI	TRUCTI DENT C	ON: FEN	CE EQUIY S POL E T	ALENT YPE = 1	USAGE: 6378. 0	OST OF	NOTHING EXPECTED ACCIDE	EXP	ECTED ROCTUENT 3970. STANDE	S PZB: 0.0	6224418 DN =	0. 49

-	•	٠	 	-	Secretaria (M.)	-CNU talkent

POLE NO,	POLE TYPE	MAXIMUM CUFYATURE	ARDT	SKID TEST	LATERAL OFFSET	РОАD ИДОТН	DISTANCE FROM CURVE START	ONISIDE	PAVEMENT DEFICIENCIES	SUPER- ELAVATION	TOTAL RR	
E	INM	0.020	37000	35	1 00	12. 0	50	IN	NONE	BAC		
FF	4. 36	7. 40 ++	1 33	2. 29 44	1.13	1.35 ++	1 55 **	6 . 85	o. 93	1 20 ++	220, 09	
	TRUCTI DENT C	- · · ·	ID BASE S POLE T						ECTED ACCIDENT 6409. STANDA	S F/A (0.1	0N = 0 0330396	0 45
POLE NO.	POLE TYPE	MAXIMUN CURVATURE	AR[/]	SKID TEST	LATERAL OFFSET	ново ИІОТН	DISTANCE FROM CUPVE STAPT	INSTOE/ OUTSIDE	PAVEMENT MEFICIENCIES	SUPER- ELAVATION	TOTAL ER	
7	MHI	0.020	37000.	35	1.60	18. 0	• 90	IN	NONE	E:AC		
FR:	4. 3క	7. 4 <u>0</u>	1 33	2, 29 ++	1. 13	1 35	1 86	6. 85	6 93	1, 20	179, 38	
	TRUCTI DENT C	ON: RIG	ID BASE : S POLE T	STEEL	USAGE 12495. C				ECTED ACCIDENT 8484. STANDA	· ·		0 43

TOTAL NUMBER OF ACCIDENTS EXPECTED PER SITE 7.98 STANDARD DEVIATION = 2.13 TOTAL COST \$113958.

```
TREATMENT ALTERNATIVE NUMBER 1
________
     TREATMENT PART NUMBER 1 RESURFACE DRAG STREET AT HAIRY CORNER
          POLE 1 SMID TEST RESULT CHANGED TO 60 NEW RELATIVE RISK 0.73
POLE 2 SKID TEST PESULT CHANGED TO 60 NEW RELATIVE RISK 0.73
POLE 3 SKID TEST PESULT CHANGED TO 60 NEW RELATIVE RISK 0.73
POLE 4 SKID TEST PESULT CHANGED TO 60 NEW RELATIVE RISK 0.73
POLE 5 SKID TEST RESULT CHANGED TO 60 NEW RELATIVE RISK 0.73
POLE 6 SKID TEST RESULT CHANGED TO 60 NEW RELATIVE RISK 0.73
POLE 7 SKID TEST RESULT CHANGED TO 60 NEW RELATIVE RISK 0.73
     NEW EXPECTED NUMBER OF ACCIDENTS PZA FOR SITE - 2.9631 CHANGE = -5 0158
     SERVICE LIFE 10 YEARS CAPITAL COST # 7875 DISCOUNTED BENEFITS # 290010.
     NET PRESENT VALUE # 290135. BENEFIT/COST RATIO = 37.84 SIANDARD DEVIATION = 27.26
     ** TREATMENT ACCEPTED **
EFFECTS OF ALTERNATIVE NUMBER 1
______
PARTS INCLUDED:
NEW EXPECTED NUMBER OF ACCIDENTS FOR SITE 2.96215 CHANGE = -5.01583
TOTAL CAPITAL COST # 7875. TOTAL BENEFITS # 298010
NFT PRESENT VALUE $ 290135. BENEFIT/COST PATIO 37.84 STANDARD DEVIATION ★ 27.26
TREATMENT ALTERNATIVE NUMBER 2
     TREATMENT PART NUMBER 2 REMOVE ALL POLES ON THE OUTSIDE OF HAIPY CORNER 1 .
           POLE 1 HAS BEEN REMOVED.
           POLE & HAS BEEN REMOVED.
                                                 CHANGED TO 4,50 NEW RELATIVE RISK 0.48
           POLE 3 LATERAL OFFSET
           POLE 3 CONSTRUCTION CHANGED TO FENCE EQUIVALENT NEW ACCIDENT COST # $ 6378.
           FOLE 4 LATERAL OFFSET CHANGED TO 2.50 NEW RELATIVE RISK 0.52
```

POLE 4 CONSTRUCTION CHANGED TO FENCE EQUIVALENT NEW ACCIDENT COST • \$ 6378.

POLAME USER MANUAL - A FUNTHER POLITY EMHAPLE UTILITY POLE SITE TREATMENT PROGRAM

PAGE : 22-DEC-80

NEW EXPECTED NUMBER OF ACCIDENTS F/A FOR SITE 3, 3687 CHANGE = -4, 6093
SERVICE LIFE 15 YEARS CAPITAL COST \$22000. DISCOUNTED BENEFITS \$ 347026.
NET PRESENT VALUE \$ 325026. EENEFIT/COST RATIO = 15, 77 STANDARD DEVIATION = 4, 52
** TREATMENT ACCEPTED **

CEPPETE OF OUT TENANT AND THE SECOND OF THE

EFFECTS OF ALTERNATIVE NUMBER &

PARTS INCLUDED:

NEW EXPECTED NUMBER OF ACCIDENTS FOR SITE 3.36868 CHANGE = -4.60930

TOTAL CAPITAL COST \$28000 TOTAL BENEFITS \$ 347020 **

NET PRESENT VALUE \$ 325026 BENGEIT/COST RATIO 15 77 STANDARD DEVIATION = 4.58

TPEATMENT ALTERNATIVE NUMBER 3

TREATMENT PART NUMBER 3 INCREASE THE LATERAL OFFSET OF POLES 3 & 4

POLE 3 LATERAL OFFSET CHANGED TO 3.00 NEW RELATIVE RISK 0.47
FOLE 4 LATERAL OFFSET CHANGED TO 2.50 NEW RELATIVE RISK 0.52
NEW EXPECTED NUMBER OF ACCIDENTS P/A FOR SITE 5.6515 CHANGE = -2.3265
SERVICE LIFE 15 YEARS CAPITAL COST \$ 2000. DISCOUNTED BENEFITS \$ 151230
NET PRESENT VALUE \$ 149230. BENEFIT/COST PATIO = 75.61 STANDARD DEVIATION = 65.02
** TREATMENT ACCEPTED **

TREATMENT PART NUMBER 4 INCREASE THE LATERAL OFFSET OF POLES 1 & 2

POLE 1 LATERAL OFFSET CHANGED TO 3.00 NEW RELATIVE RISK 0.47

POLE 2 LATERAL OFFSET CHANGED TO 3.00 NEW RELATIVE RISK 0.47

NEW EXPECTED NUMBER OF ACCIDENTS P/A FOR SITE 4.1994 CHANGE = -1.4581

SERVICE LIFE 15 YEARS CAPITAL COST # 2000. DISCOUNTED BENEFITS # .94394.

NET PRESENT VALUE # .92394. BENEFIT/COST PATIO = .47.20 STANDARD DEVIATION • .67.01

** TREATMENT ACCEPTED ***

4, 52

EFFECTS OF ALTERNATIVE NUMBER 3

PARTS INCLUDED:

4

3. 3687

NEW EMPECTED NUMBER OF ACCIDENTS FOR SITE 4.19938 CHANGE = -3.77859

\$22000

TOTAL CAPITAL COST # 4000. TOTAL BENEFITS # 245624

NET PRESENT VALUE # 841624 BENEFIT/COST KOTIO 61 41 STANDARD DEVIATION F 45 97

325026.

15, 77

RESULTS FOR SI	ITE 9.		•	•		
ALTERNATIVE NUMBER	EMPECTED ACCIDENTS PZA	CAPITAL COST	TOTAL BENEFITS	NET PRESENT VALUE	BENEFIT/COS? RATIO	STANDARD DEVIATION
3	4, 1994	≇ 4000 .	≇ 245624.	# 241624	61. 41	45, 97
1	2 9621	# 7 875.	\$ 298010.	\$ 290135 ·	37, 84	27, 26

\$ 347036.

-112

APPENDIX F

ACCIDENT COSTING

Accident costs used in the POLFIX program are based on work done by FOX et al. (1)

Several methods have been proposed for determining the cost of accidents. After a short summary of the most common approaches the costs used in POLFIX will be discussed.

There are two common approaches to assigning accident costs:

- a) Ex-poste, and
- b) Ex-ante

The ex-poste method is one which reviews the cost elements after the event. The ex-ante approach attempts to assess what society is willing to pay for a given reduction in the probability of an accident. POLFIX uses the ex-poste method.

Accident costs may be classified into two major groups:

- a) direct costs, and
- b) indirect costs.

Indirect costs include the value of pain and suffering and losses in production by others as a result of the accident.

Direct costs may be further classified as:

- a) Use of current resources, and
- b) Loss of future production.

Current resources consumed as a result of an accident include property damage repairs, medical and hospital treatment, legal charges, insurance and police costs. Loss of future production occurs in the case of death or permanent disability. This may be modified by subtracting an estimate of future consumption.

Accident Costing Methods Adopted

The approaches adopted in the majority of accident cost studies fall into three main groups.

CRC: Current resource costs only,

TCNC: Total accident costs, including loss of future production

net of consumption,

TC: Total accident costs, including loss of future production.

(1) FOX, J.C, GOOD, M.C., and JOUBERT, P.N. (1979)
"Collisions with Utility Poles", <u>Australian Department of Transport</u>,
Report CR1.

The total accident cost (TC) approach was adopted for POLFIX. components included in the total accident cost are:

- o Loss of future production,
- o Loss of services to home, family and community,
- o Medical,
- o Legal and court,
- Insurance administration,
- o Accident investigation,
- Losses to others,
- Vehicle damage,
- o Traffic delay,o Pole and utility damage.

The cost of pain and suffering is not included, which makes the estimate of accident costs conservative.

Fox et al estimated accident costs for different injury levels. Since utility pole construction and accident severity are correlated, accident costs can be estimated for different types of pole.

Accident costs are continually changing with inflation. POLFIX attempts to solve this problem by applying the Consumer Price Index to accident cost figures. The initial estimates of cost were in 1977 Australian dollars. POLFIX automatically indexes accident costs to the current year. In order to do this an estimated future inflation rate of 8% per armum is included. This is a conservative estimate. A list of the costs adopted for different pole types may be found in Appendix C.

TREATMENT COSTING

The cost of implementing remedial treatments will vary according to the SITE being treated. POLFIX has a list of standard treatments and costs. Treatments in the list may be selected by using a numeric treatment code. Details of the standard treatments are listed in Appendix C.3.

If standard treatments do not apply, the user must supply costing information for the treatment, such as:

- a) Capital cost per unit of treatment,
- b) Service life of the treatment,
- c) Number of units included in this treatment, and
- d) The annual maintenance cost (if any).

After gaining experience in using the package, the user may wish to update the list of standard treatments in the POLFIX program. The POLAXE Programmer's Guide should be consulted before attempting to change the standard treatments.

Cost benefit analysis is used by the POLFIX program to discriminate between alternative remedial treatments. Discounted present value techniques are used to achieve this goal. The basis of this technique is that a given sum of money is worth more now than at some future year. This is because the money may be invested now and yield returns in future years. To calculate the present value of a future year payment, the payment is multiplied by a present worth (p w) factor. The formula for determining this factor is

$$p w_{p} = 1/(1 + r)^{n}$$

Where n is the future year

r is the investment interest rate

To obtain the present worth of a steady flow of money, i.e. yearly payments each payment should be multiplied by the present worth factor for that year and the results summed.

POLFIX has adopted the following definitions of costs and benefits:

COSTS - The capital outlay required for the construction of the improvement.

BENEFITS - are defined to be the savings accruing from the reduction in number and/or severity of accidents attributable to the treatment

minus

Annual maintenance costs of the improvement.

One problem in economic analysis of remedial treatments is that alternative treatments may have different service lives. The approach POLFIX adopts is to evaluate all treatments over a period of five years. A five-year period was chosen as the forseeable future. The choice of a relatively small figure ensures that POLFIX is conservative in its predictions.

- 1. The present value of 5 yearly payments of one dollar is calculated for the specified interest rate.
- 2. The yearly flow of accident cost saving is calculated as the previous cost of site accidents minus the current cost of site accidents.
- 3. The yearly flow of accident cost savings are multiplied by the discount factors to give the present worth of 5 years accident savings.

- 4. The annual flow of maintenance cost is also multiplied by the discount factors.
- 5. The total present value of benefits is calculated as the present value of accident savings minus the present value of maintenance costs.
- 6. Since the capital cost is outlaid immediately, no discounting is needed.
- 7. The Net Present Value of a treatment is the present value of benefits minus the capital cost.
- 8. The Benefit Cost Ratio is the present value of benefits divided by the capital cost.

RISK ANALYSIS

I.1 Estimation of Confidence Limits for Risk Factors

This section shows the method of calculating confidence limits for the relative risk factors. A worked example is also presented. For simplicity the MNI model will be considered in the following although the results are general. Three equations are of interest in calculating expected accident rates.

i.e. - the risk factor for a pole equals the product of the individual relative risk components.

This calculation of risk factor assumes that the variables have independent effects on the probability of a pole accident.

i.e. - the total relative risk for a pole in the MNI group is the product of the risk factor within the data group and the relative risk of that group compared to other data groups.

3)
$$\gamma = TRR * \bar{p}T$$

i.e. - the expected number of accidents per annum equals the total relative risk by the mean probability \bar{p} that a pole record trial will result in an accident by the number of trials T in a year.

Confidence limits of 68% are available for the individual relative risk factors. Confidence limits are not available for the relative risk of a data group (RR^{MNI}) or the pole trial probability (\bar{p}). These are assumed to be exactly known.

To calculate the standard deviation of the total relative risk only the individual standard deviations of the relative risks of poles within a group (e.g. MNI), will be considered. It will be assumed that the component relative risk values are independent and not related. In addition, a normal distribution of error will be assumed. The assumptions in summary are therefore, that:

- errors of relative risk for poles within a group are normally distributed and independent.
- p and RRMNI are known exactly.

Using these assumptions the following formula can be derived:

⁽¹⁾ For a full treatment of relative risk calculations see FOX, J.C., GOOD, M.C., and JOUBERT, P.N. (1979) "Collisions with Utility Poles", <u>Australian Department of Transport Report No. CR1. Chapter 4.</u>

4)
$$V(xyz...) = E(x^2)E(y^2)E(z^2).... - \mu x^2 \mu y^2 \mu z^2$$

where $E(x^2) = V(x) + \mu^2 x$

I.2 Example Confidence Limit Calculation

Variable	RR	rr ²	Standard Deviation	Variance . of RR
_{RR} MNI	4.36	19.0096	exact	0
KMAX	3.11	9.672	0.57	.33
AADT	1.24	1.538	0.15	.023
ST	1.50	2.25	0.18	0.032
ro	1.38	1.904	0.09	0.008
₩ .	1.32	1.742	0.11	0.012
DC	1.12	1.254	0.59	0.349
PD	2.00	4.0	.6	.36
e	1.20	1.44	exact	0
IOB	1.15	1.323	exact	0

TRR = product of RR's = 142.02

$$\gamma$$
 = TRR * \bar{p} T = .536

From the above formula

Standard deviation = 100.39

Therefore the total relative risk is 142.02 with a standard deviation of 100.38. The 68% confidence limits on this value of TRR are 41.64 to 242.40. The expected number of accidents per annum is .536 with a standard deviation of 0.379. The standard deviation of the expected number of accidents per annum may optionally be included on PRANK and POLFIX reports.

I.3 Estimation of Confidence Limits for Benefit-Cost Ratios

For a site with n = 1,2,3... poles the benefit-cost ratio is calculated for the $i \le n$ poles being treated. The remaining (n-i) poles maintain their untreated accident expectancies and costs, assuming the accident risk of a pole is independent of the pole's proximity to other poles.

The benefit cost(BC) ratio is expressed as

$$BC = \frac{(a_1c_1 - a_2c_2 - M)}{t} pwf$$

where a_1 = number of accidents for untreated pole

 c_1 = cost of accidents for untreated pole

a₂ = number of accidents for treated pole

 c_2 = cost of accidents for treated pole

t = treatment cost

pwf = present worth factor (see Appendix G)

M = Annual maintenance cost

Accident costs c_1 and c_2 vary depending on the pole's construction and hence its accident severity.

Simplifying:

BC =
$$(a_1c_1 - a_2c_2-m)K = (a_1c_1-a_2c_2)K - mK$$

where $K = \underbrace{-pwf}_{t}$

and mK is regarded as a constant for the purpose of calculating the variance.

The variance of the variable $(a_1c_1-a_2c_2)$ can be simply calculated if it is assumed that a_1c_1 and a_2c_2 are independent. Furthermore, since variances are known for a_1 and a_2 it is assumed that c_1 and c_2 can be regarded as constants for each a_1 and a_2 .

Therefore from standard formulae:

$$Var(BC) = (c_1^2 Var(a_1) + c_2^2 Var(a_2))K^2$$

where Var(a₁) = variance of total relative risk as calculated in the previous section.

For n poles in a site, i of which are treated in some way, the benefit cost calculation for the site is as follows:

6) BC
$$\{\sum_{j=1}^{i} a_{j} \circ c_{j} \circ - \sum_{j=1}^{i} a_{j} \circ c_{j} \} *K - \sum_{j=1}^{i} M_{1} K_{1}$$

7) Var (BC) =
$$K^2 \{\sum_{j=1}^{1} (c_j^2 o Var(a_{jo}) + c_j^2 Var(a_{jm}))\}$$

where o (original) denotes accidents and costs pri

where o (original) denotes accidents and costs prior to treatment,

and m (modified) denotes accidents and costs after treatment.

The standard deviation of Benefit Cost is calculated by and listed in the output of POLFIX.

I.4 Example Calculation of Benefit Cost Variance

Consider a site with three poles; one pole is moved laterally, one pole converted to wrap-around construction and one pole is untouched.

Description	Pole 1	Pole 2	Pole 3
Accidents P/A	4.6	1.4	1.4
Variance	5.9	.5	.5
Cost per accident	\$20,000	\$10,000	\$10,000
Total accident cost	\$92,000	\$14,000	\$14,000
Treatment	increase lateral offset	wrap-around	none
Treatment cost	\$ 5,000	\$ 4,000	-
New number of accidents P/A	1.6	1.4	1.4
Variance	. 4	.5	.5
New cost per accident	\$20,000	\$ 5,000	\$10,000
Annual maintenance cost	\$ 0	\$ 0	\$ 0
Present worth factor for 5 years @ 10%	4:17	4.17	4.17

The benefit cost is then:

BC =
$$((4.6*20,000)+(1.4*10,000)-(1.6*20,000)-(1.4*5,000))*(4.17/9000)$$

= $106000 - 39000*(4.17/9000)$

= 31.04

$$Var(BC) = (4.17/9000)^{2} \{ (20000^{2} * 5.9) + (10000^{2} \times 0.5) + (20000^{2} * 0.4) + (5000^{2} * 0.5) \}$$

$$= 554.41$$

The standard deviation is then 23.46.

Therefore, one standard deviation (or 68%) confidence limits for the benefit cost are 31 ± 23 .

RELATIVE RISK PLOTS

The following relative risk plots are included:

Major Road Non-Intersection (MNI) Model

<u>Variable</u>	Figure or Table
Absolute maximum curvature	F/J.4
Annual average daily traffic	F/J.5
British pendulum skid test result	F/J.5
Lateral offset of the pole	F/J.7
Distance between curbs (undivided roads) F/J.8
Distance from curve start	F/J.9
Pavement deficiencies	T/J.3
Superelevation of the curve	T/J.4
Pole on inside or outside of bend	T/J.5

Minor Road Non-Intersection (MINI) Model

<u>Variable</u>	Figure or Table
Absolute maximum curvature	F/J.10
Grade at 30m upstream of pole	F/J.11
British pendulum skid test result	F/J.12
Lateral offset of pole	F/J.13
Road Width	F/J.14
Pole on inside or outside of bend	F/J.6

Intersection of Major Roads (MJMJ) Model

<u>Variable</u>	Figure or Table
Intersection type	T/J.8
Annual average daily traffic roadway 1	F/J.15
British pendulum skid test, roadway 1	F/J.16
Lateral offset of the pole	F/J.17
Annual average daily traffic, intersecting roadway 1	F/J.18
Roadway 1 divided/undivided	T/J.7
Intersecting roadway divided/undivided	T/J.7
Grade 30m upstream of intersection on roadway 1	F/J.19

Intersection of Major and Minor Roads (MJMI) Model

<u>Variable</u>	Figure or	Table
Intersection type	T/J.10	
Annual average daily traffic roadway 1	F/J.20	
British pendulum skid test result roadway 1	F/J.21	
Lateral offset of pole	F/J.22	
Distance between curbs, intersecting roadway	F/J.23	
Roadway 1 divided/undivided	T/J.9	
Grade 30m upstream of the intersection on roadway 1	F/J.24	
Radial distance of pole from centre of intersection	F/J.25	

Figure J.1 - deleted

Figure J.2 - deleted

Figure J.3 - deleted

Table J.1 - deleted

Table J.2 - deleted

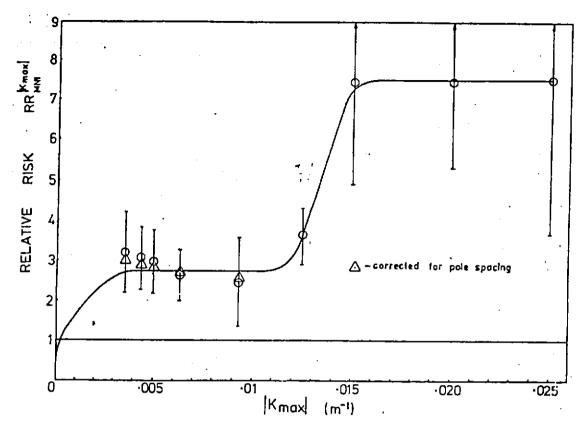


Figure J.4 Relative risk versus absolute maximum curvature upstream of the pole - MNI data group

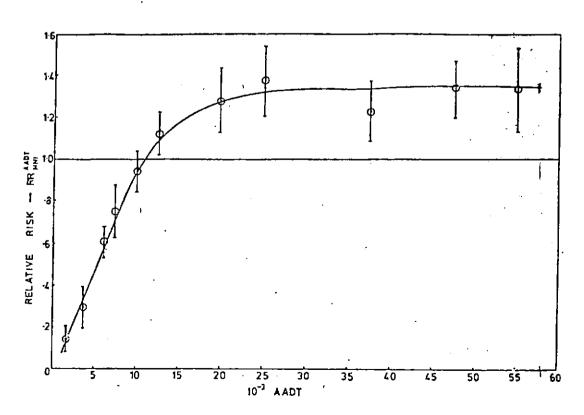


Figure J.5 Relative risk versus AADT - MNI data group

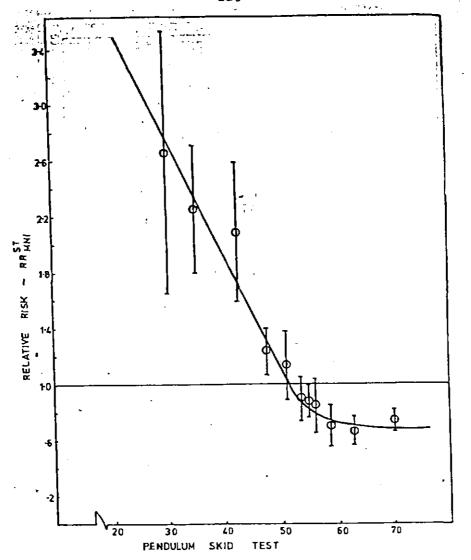


Figure J.6 Relative risk versus British pendulum skid test - MNI data group

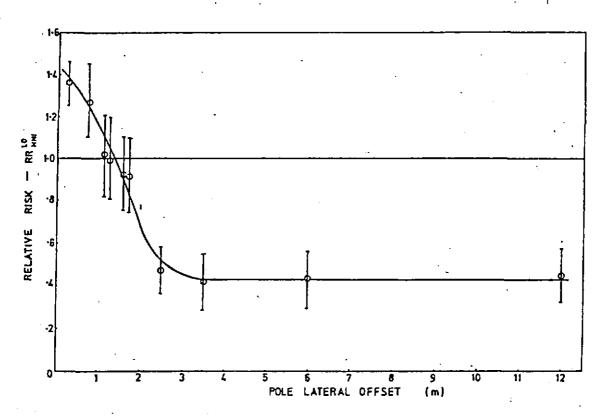


Figure J.7. Relative risk versus pole lateral offset - MNI data group

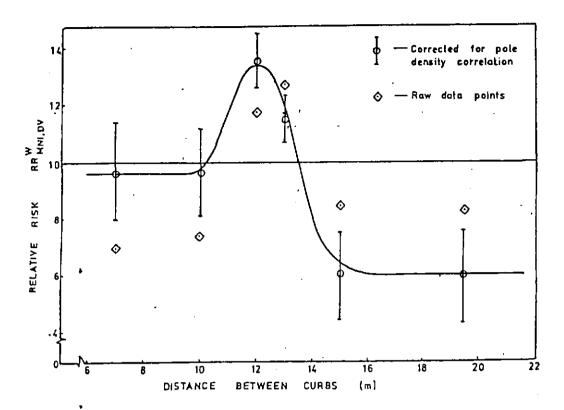


Figure J.8.Relative risk versus distance between curbs (road width) for undivided roads - MNI data group

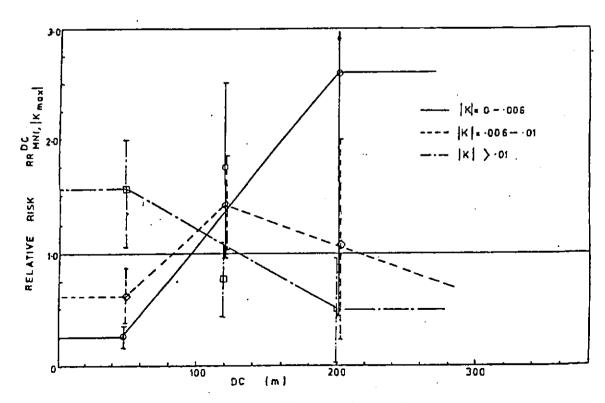


Figure J.9. Relative risk versus distance from curve start controlling for absolute maximum curvature - MNI data group

Pavement deficiency	Relative Risk	Standard Deviation
Hone	0.93	0.04
Tram tracks	0.99	0.17
Dip/Crest	1.89	0.60
Corrugations, holes	2.00	0.60

table J.4. $\mbox{ relative risk for superelevation given curvature } (\mbox{ } \mbox{ } \m$

Curvature	Calculated RR Superelevation		Selected RR <mark>e</mark> Superelevation	
	<u>-</u>	+	-	+
Left	0.93	1.23	0.9	1.2
Right	. 1.22	0.78	1,2	0.9

TABLE J.5

RELATIVE RISKS ASSOCIATED WITH POLES ON THE INSIDE AND OUTSIDE OF CURVES --

MNI DATA GROUP

		-
Location of Pole	Relative Risk	_
Inside Outside	0.85 1.15	

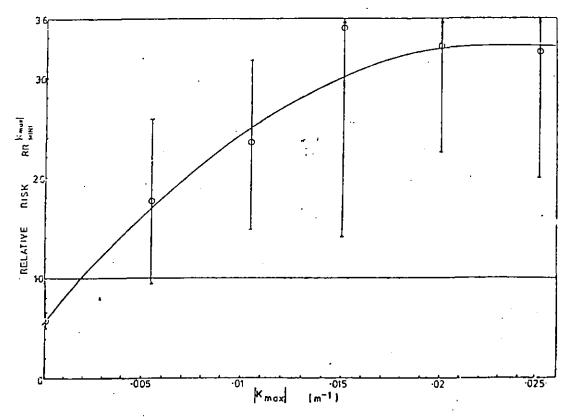


Figure J-10. Relative risk versus absolute maximum curvature upstream of the pole – MINI data group

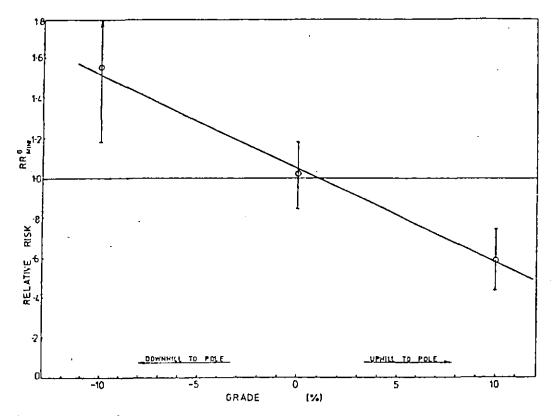


Figure J.11. Relative risk versus grade 30m upstream of the pole - MINI data group

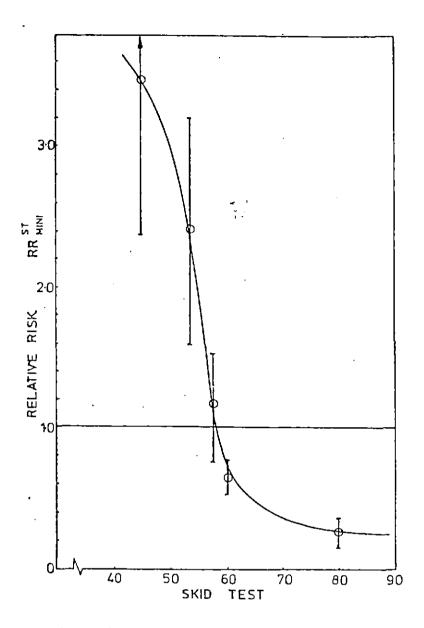


Figure J.12.Relative risk versus skid test = MINI data group

TABLE J.6

RELATIVE RISK VERSUS LOCATION OF POLE ON A CURVE -- MINI DATA GROUP

	SD
Inside of curve 1.29 Outside of curve 0.76	

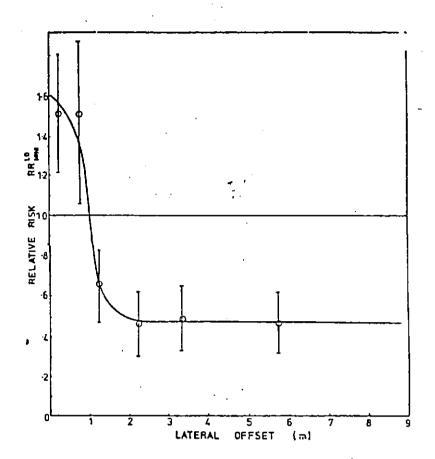


Figure J.13.Relative risk versus pole lateral offset - MINI data group

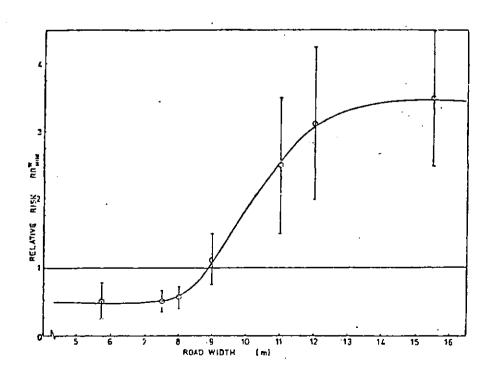


Figure J_14. Relative risk versus road width - MINI data group

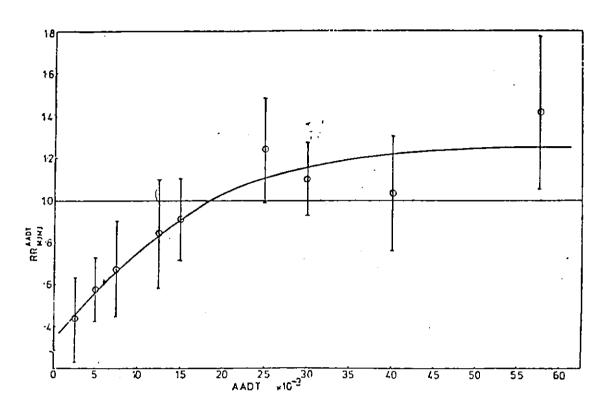


Figure J.15. Relative risk versus AADT on roadway 1 - MJHJ data group

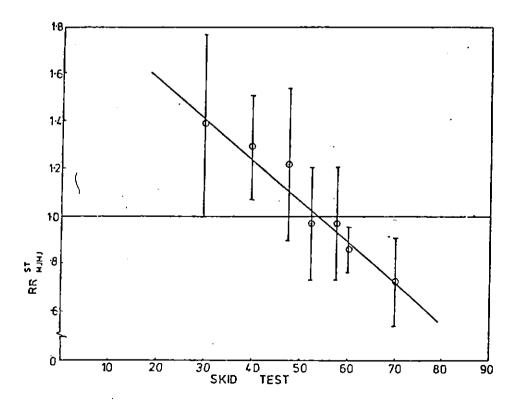
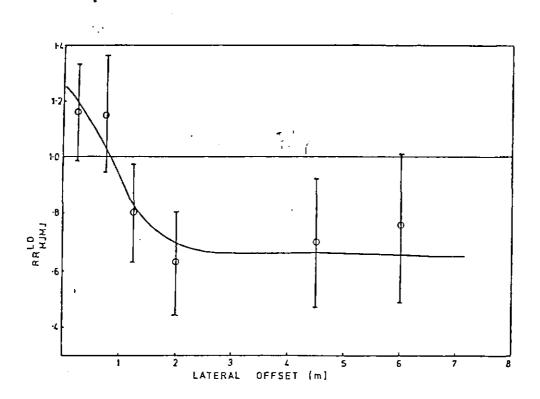


Figure J.16. Relative risk versus skid test on roadway 1 - MJMJ (intersection) data group



'Figure J.1% Relative risk versus pole lateral offset - MJMJ data group

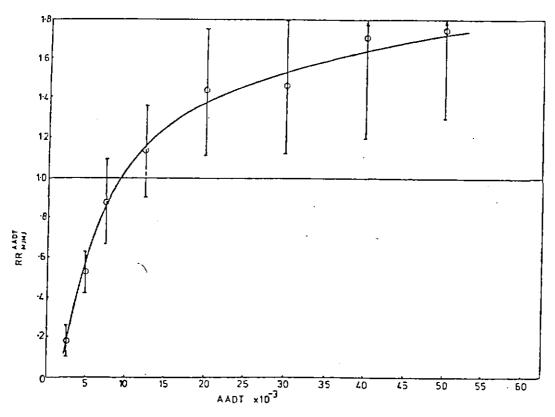


Figure J.18.Relative risk versus AADT on the intersecting roadway - MJMJ data group

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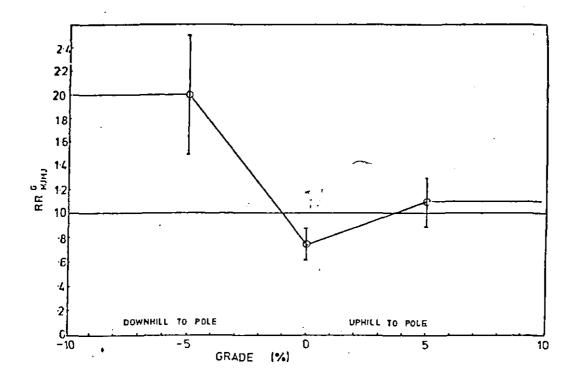


Figure $J.19.\,\mathrm{Relative}$ risk versus grade of roadway 1, 30m before the intersection - MJHJ data group

TABLE J.7

CHOSEN VALUES OF RELATIVE RISK AGAINST BOTH INTERSECTING ROADWAYS

DIVIDED/UNDIVIDED CONTROLLING FOR THE PRESENCE OF TRAFFIC LIGHTS -- MJMJ

Roadway Divided/Undivided	Relative Risk		
	Traffic Lights	Other	
Divided	1.00	0.11	
Undivided	1.00	1.80	

TABLE J. 8

RELATIVE RISKS FOR CROSS AND TEE INTERSECTIONS, CONTROLLING FOR PRESENCE
OF TRAFFIC LIGHTS -- MJMJ

Type of control		
Traffic lights	No traffic lights	
1.0	1.9	
	Traffic lights RR 1.0	

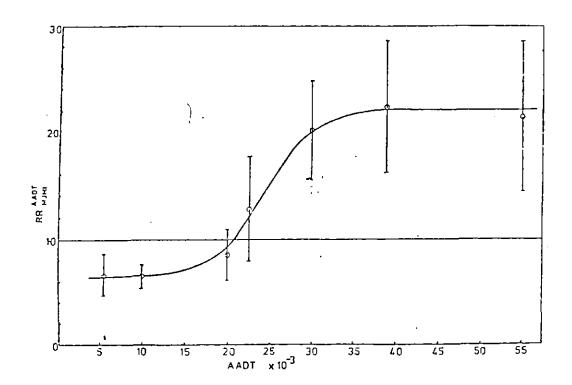


Figure J. 20. Relative risk versus AADT on the major road - MJMI data group

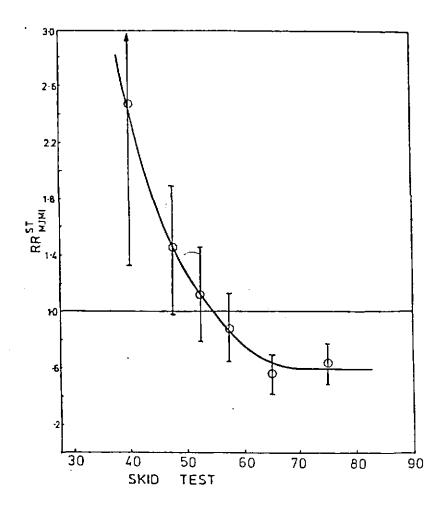


Figure J.21. Relative risk versus British pendulum skid test on the major road - MJMI data group

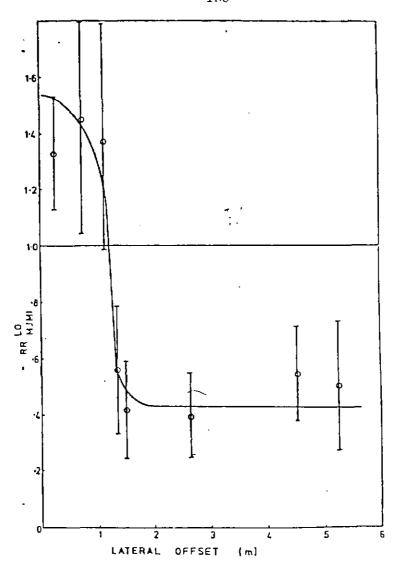


Figure J. 22, Relative risk versus pole lateral offset - MJMI data group

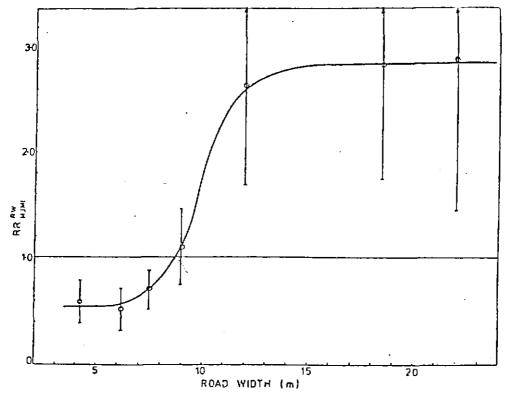


Figure J.23. Relative risk versus width of intersecting minor roadway - MJNI data group

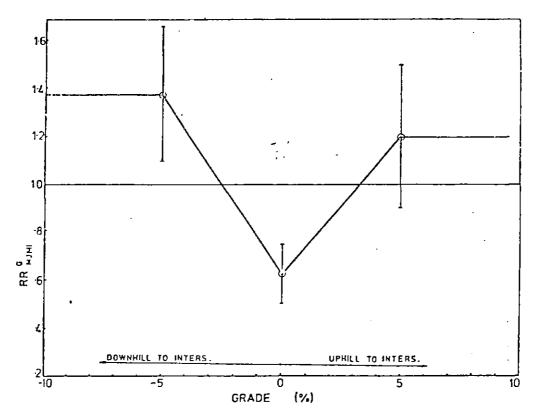


Figure J. 24.Relative risk versus grade of the major road 30m before the intersection - MJMI data group

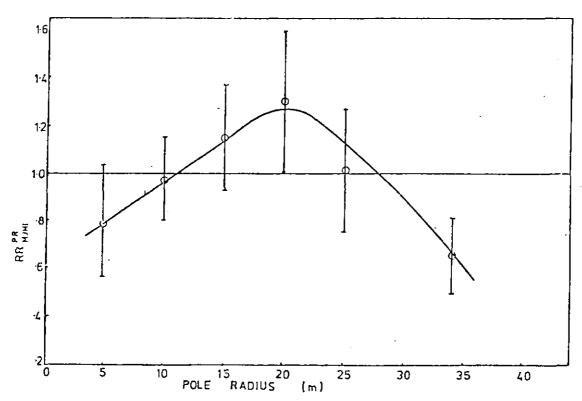


Figure J.25. Relative risk versus radial distance of the pole from the centre of the intersection - MJMI data group

TABLE J.9 .

RELATIVE RISK FOR ROADWAY 1 DIVIDED/UNDIVIDED -- MJMI DATA GROUP

Roadway Divided/Undivided	RR	SD
Divided Undivided	0.5B 1.43	0.21

TABLE J.10

RELATIVE RISK BY INTERSECTION TYPE (+ OR T) MJMI DATA GROUP

Intersection Type	RR	SD		
+	2.50	0.53	•••	
7	0.70	0.13		

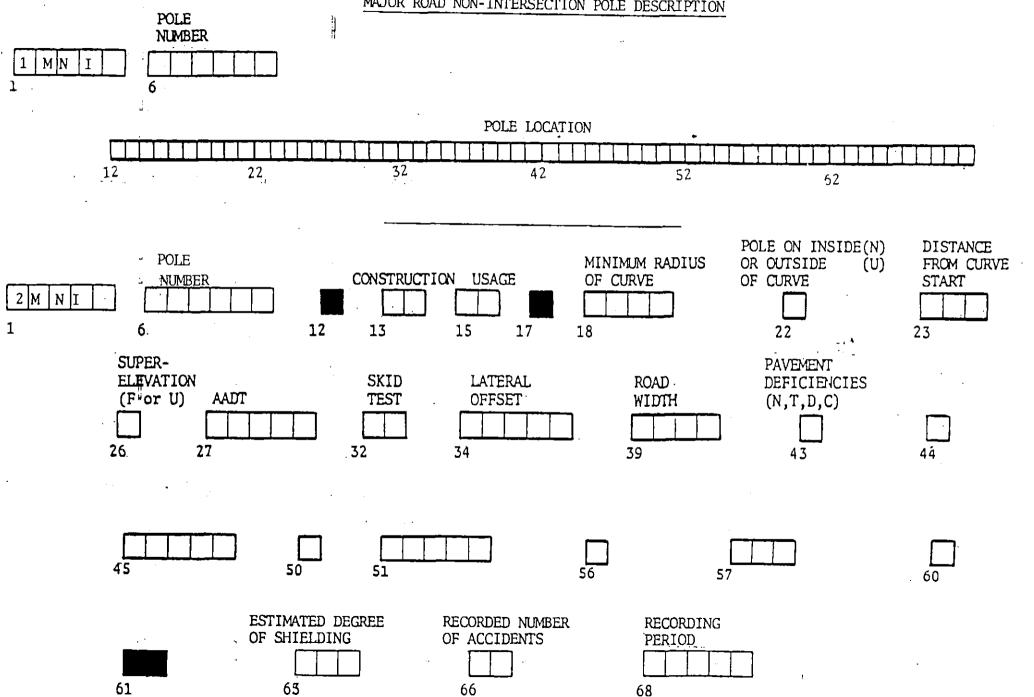
APPENDIX K

SAMPLE POLE INPUT FORMS

A copy of each pole input form is included for the user to copy.

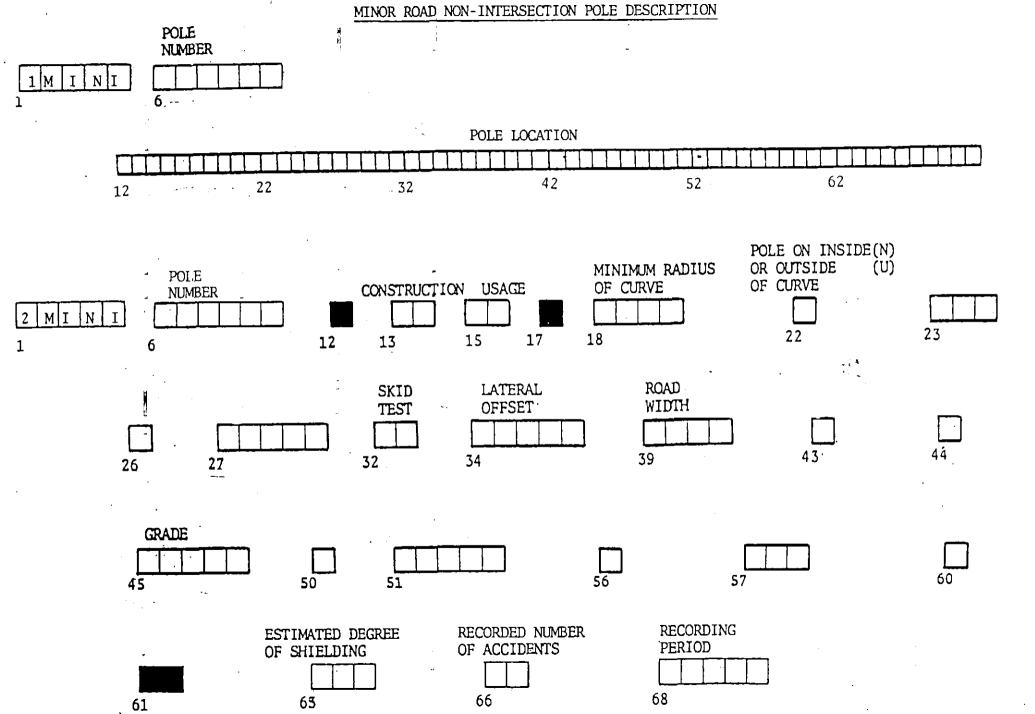
-140-

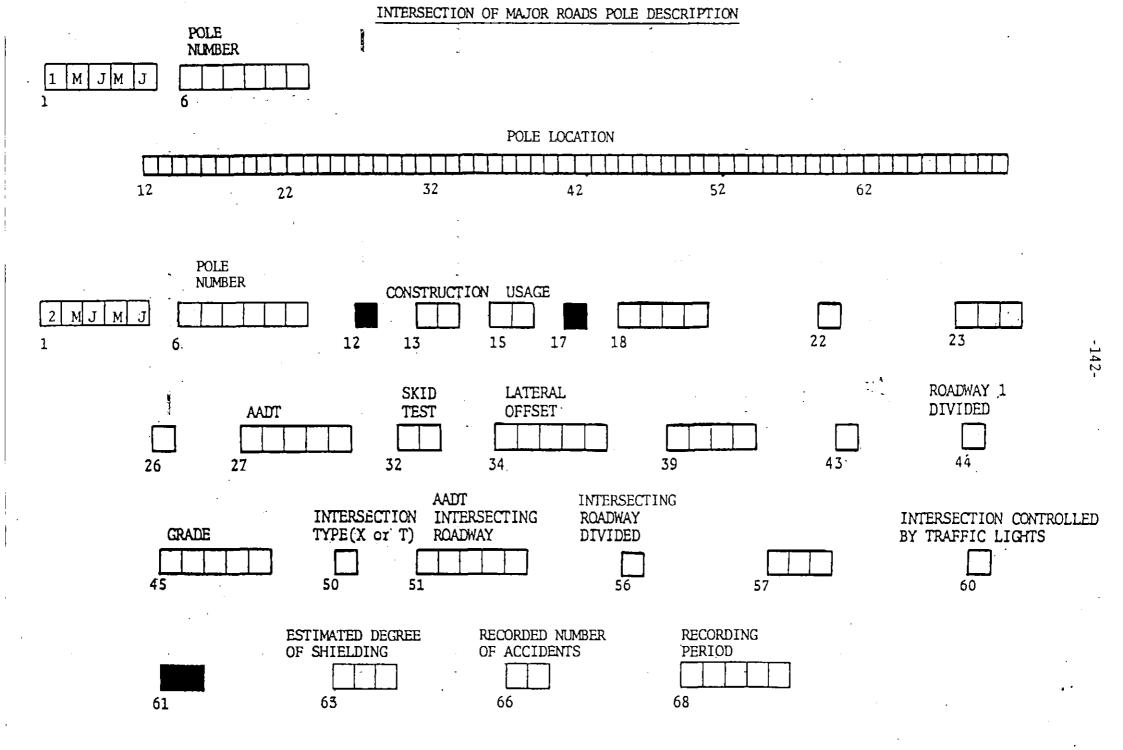
MAJOR ROAD NON-INTERSECTION POLE DESCRIPTION



PR-2

-141-





66

61

65

68

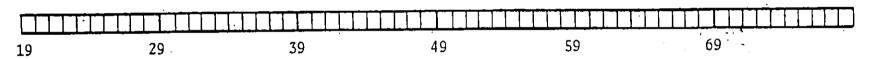
-143-

OPTIONS AND PARAMETERS

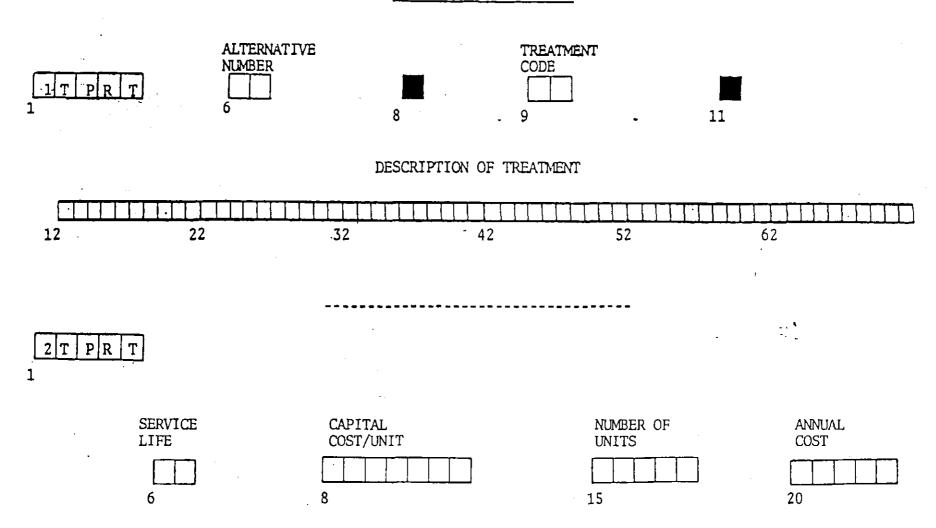
PRINT REPORT SORTED BY FULL SORTED UNSORTED FULL UNSORTED EXPECTED NUMBER OF ACCIDENTS REPORT REPORT REPORT (Y or N) (Y or N) (Y or N) (Y or N) OP READ RECORDED SKID TESTER PRINT STANDARD B = BRITISH PORTABLE **ACCIDENTS** DEVIATIONS (Y or N) S = SCRIM(Y or N) 12 10 HEADING FOR OUIPUT 54 64 34 44 14 24 RELATIVE RISK BY POLE CATEGORIES 2 O P T N MAJOR/MAJOR MAJOR/MINOR MINOR ROAD MAJOR ROAD INTERSECTION INTERSECTION NON INTERSECTION NON INTERSECTION 21 11 16 ACCIDENT CUTOFF NUMBER FACTOR OF ACCIDENTS 34 26

SITE NUMBER SITE BUDGET 1 S I T E 6 10 12 18

SITE DESCRIPTION



TREATMENT DESCRIPTION

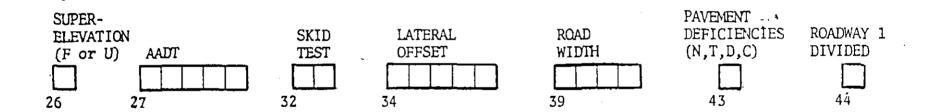


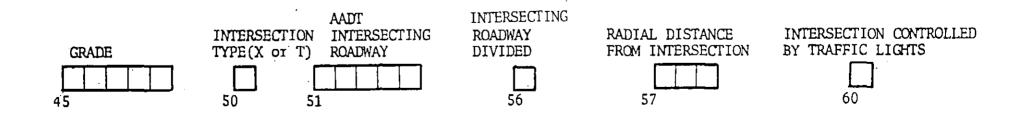
TREATMENT EFFECT FORM

Only fill in fields that have changed

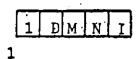
TE FF

					POLE ON INSIDE(N)	DISTANCE .
SITE	POLE			MINIMUM RADIUS	OR OUTSIDE (U)	FROM CURVE
NUMBER	NUMBER	CONSTRUC	TION USAGE	OF CURVE	OF CURVE	START
6	10	12 13	15 17	18 ·	22	23

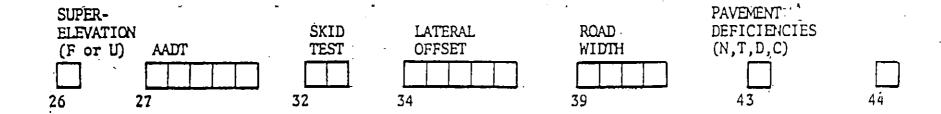




MAJOR ROAD NON-INTERSECTION POLE DESCRIPTION

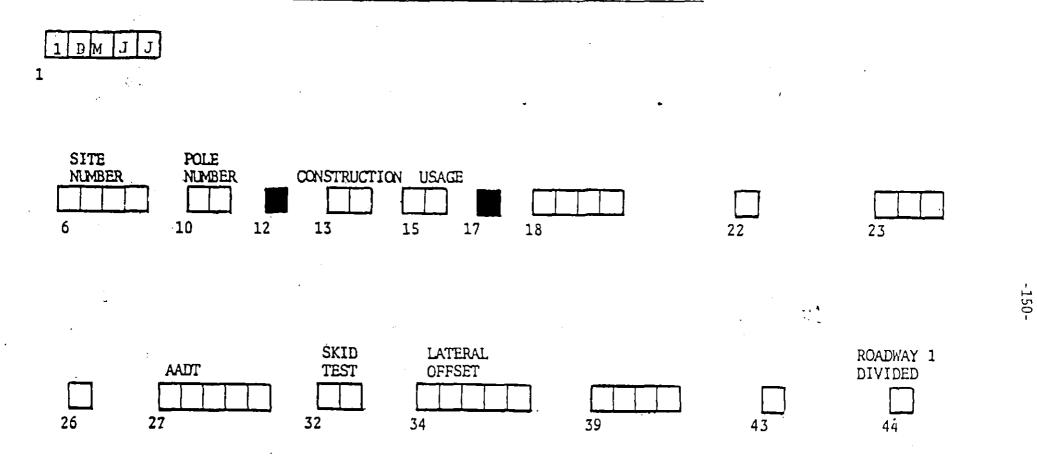


POLE ON INSIDE(N) DISTANCE OR OUTSIDE FROM CURVE SITE POLE MINIMUM RADIUS (U) · OF CURVE START CONSTRUCTION USAGE OF CURVE NUMBER. NUMBER 23 .10 12 13 15 18 22 6 17

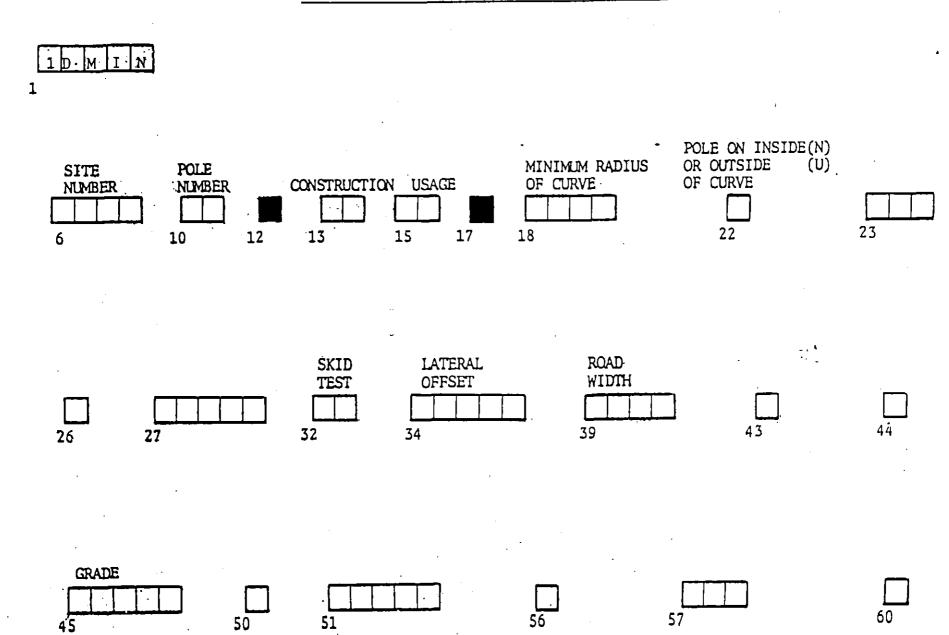




DESCRIPTION OF POLE AT INTERSECTION OF MAJOR ROADS



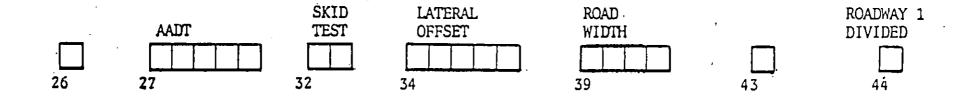
GRADE	AADT INTERSECTION INTERSECTING TYPE(X or T) ROADWAY	INTERSECTING ROADWAY DIVIDED		INTERSECTION CONTROLLED BY TRAFFIC LIGHTS
45	50 51	56	57	60



DESCRIPTION OF POLE AT INTERSECTION OF MAJOR & MINOR ROADS

. 1 DM J I

SITE	POLE				•			
NUMBER	NUMBER		CONSTRUCTIO	ON USA	Œ	- ·		
6	10	12	13	15	17	18	22	23





-7CT